

Table 3. Kinetics methods used in WT pyrolysis mechanism's study

Method	General Equation	Description
Model-fitting methods		
Coats-Redfern Method	$\ln \frac{g(\alpha)}{T^2} = \ln \left(\frac{AR}{\beta E_a} \left[1 - \left(\frac{2RT_{exp}}{E_a} \right) \right] \right) - \frac{E_a}{RT} \quad (20)$	A plot of $\ln \frac{g(\alpha)}{T^2}$ against $1/T$ for low values of α , should be a straight line with a slope of $-E/R$ since $\ln \left(\frac{AR}{\beta E_a} \left[1 - \left(\frac{2RT_{exp}}{E_a} \right) \right] \right)$ is sensibly constant. The activation energy and A are obtained from the slope, and the intercept, respectively and the model that gives the best linear fit is chosen as the model.
Direct differential method	$\ln \frac{d\alpha/dT}{f(\alpha)} = \ln \frac{A}{\beta} - \frac{E_a}{RT} \quad (21)$	Plotting the left-hand side (including the model) versus $1/T$ gives the E_a and A from the slope and y intercept, respectively. The model that gives the best linear fit is usually chosen as the model.
Freeman-Carroll Difference-Differential	$\frac{\Delta \ln \frac{d\alpha}{dT}}{\Delta 1/T} = \frac{\Delta \ln f(\alpha)}{\Delta 1/T} - \frac{E_a}{R} \quad (22)$ $\text{or } \frac{\Delta \ln \frac{d\alpha}{dT}}{\Delta 1/T} = -\frac{E_a}{R} \frac{\Delta 1/T}{\Delta \ln f(\alpha)} \quad (23)$	The activation energy is obtained by plotting the left-hand side of Eq. (22) and Eq. (23) versus $\frac{\Delta \ln f(\alpha)}{\Delta 1/T}$ and evaluating the intercept for Eq. (22) or versus $\frac{\Delta 1/T}{\Delta \ln f(\alpha)}$ and evaluating the slope for Eq. (23).
Model-free methods		
Friedman's isoconversional method	$\ln \left(\beta \frac{d\alpha}{dt} \right)_\alpha = \ln A_\alpha + \ln f(\alpha) - \frac{E_{a\alpha}}{RT_\alpha} \quad (24)$	Plotting $\ln \left(\beta \frac{d\alpha}{dt} \right)$ versus $1/T$ at given reaction progress, α , for various heating rates yields a straight line with slope $-E_a/R$. The E_a can be obtained from this slope without knowing the reaction function $f(\alpha)$. The pre-exponential factor A is the y-intercept of the straight line.
Ozawa method	$\ln \beta = \ln \left(\frac{AE}{g(\alpha)R} \right) - 5.330 - 1.052 \frac{E}{RT} \quad (25)$	Provided that $g(\alpha)$ is constant at a given value of α , the slope of the plots of $\ln \beta$ vs the reciprocal of the temperature for particular values of α lead to the activation energy as a function of α , independently of the kinetic model fitted by the reaction.
Kissinger method	$\ln \left(\frac{\beta}{T_m^2} \right) = \ln \left(\frac{AR}{f(\alpha)} \right) - \frac{E_a}{RT_m} \quad (26)$	A plot of $\ln \left(\frac{\beta}{T_m^2} \right)$ versus $1/T_m$, at various heating rates yields a straight line that allows determination of the E_a from the gradient of the straight line, $\frac{-E_a}{R}$. The y-intercept serves to estimate the pre-exponential reaction rate factor.
Kissinger-Akira-Sunose (KAS) method	$\ln \left(\frac{\beta}{T^2} \right) = \ln \left(\frac{AR}{E_a} \right) - \ln g(\alpha) - \frac{E_a}{RT} \quad (27)$	The plot of $\ln \left(\frac{\beta}{T^2} \right)$ vs $1/T$ for a constant value of α will develop a straight line. The E_a is determined by the gradient of the curve, represented by $-E/R$ through multiplication with gas constant, R .
Ozawa-Flynn-Wall (OFW) method	$\ln \beta = \ln \left(\frac{AE_a}{R} \right) - \ln g(\alpha) - 5.3305 - 1.052 \left(\frac{E_a}{RT} \right) \quad (28)$	For α constant, a plot of $\ln \beta$ vs $1/T$ obtained from thermal curves recorded at several heating rates should be a straight line whose slope allows evaluation of the E_a . The pre-exponential factor value can be obtained from the intercept if the form of the integral function $g(\alpha)$ is known.
Starink Method	$\ln \left(\frac{\beta}{T^{1.8}} \right) = C_s - 1.0037 \left(\frac{E_a}{RT} \right) \quad (29)$	Starink's activation energy is obtained from the slope of $\ln \left(\frac{\beta}{T^{1.8}} \right)$ against $1/T$ whilst C_s is a constant independent of β and T .